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Direct measurement of the oceanic carbon monoxide flux by eddy correlation

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Abstract. This report presents results from a field trial of ship-based air–sea flux measurements of carbon monoxide (CO) by direct eddy correlation with an infrared-laser trace gas analyzer. The analyzer utilizes Off-Axis Integrated-Cavity-Output Spectroscopy (OA-ICOS) to achieve high selectivity for CO, rapid response (~ 2 Hz) and low noise. Over a two-day sea trial, peak daytime seawater CO concentrations were ~ 1.5 nM and wind speeds were consistently 10–12 m s⁻¹. A clear diel cycle in CO flux with an early afternoon maximum was observed. An analysis of flux error suggests the effects of non-stationarity are important, and air–sea CO flux measurements are best performed in regions remote from continental pollution sources.

1 Introduction

Carbon monoxide (CO) is produced in the ocean surface mixed layer by photolysis of chromophoric dissolved organic matter (CDOM) (Wilson et al., 1970; Lamontagne et al., 1971; Zuo and Jones, 1995). Daytime photolytic production and continual consumption by microbes (Conrad and Seiler, 1980, 1982) leads to a pronounced diel cycle in surface seawater CO concentration, with a pre-dawn minimum and an early afternoon maximum (Lamontagne et al., 1971; Conrad et al., 1982; Johnson and Bates, 1996; Stubbins et al., 2006; Zafiriou et al., 2008). Considerable variability is possible in both the rate of production (Valentine and Zepp, 1993; Zuo and Jones, 1995) and rate of consumption (Jones, 1991; Jones and Amador, 1993; Johnson and Bates, 1996). In two detailed studies of the water column CO budget, ventilation to the atmosphere was less significant than loss to microbial consumption (Bates et al., 1995; Zafiriou et al., 2003).

Although marine emissions represent a minor fraction of the global CO budget (Bates et al., 1995; Stubbins et al., 2006), the ocean may be a significant source of CO to the remote marine boundary layer in the Southern Hemisphere (Erickson and Taylor, 1992). In addition, CO is recognized as a useful tracer for studies of sea surface mixed layer processes because it couples to biological, photochemical, and physical mixing dynamics (Najjar and Erickson III, 1995; Zafiriou et al., 2008).

Due to the lack of a suitable direct flux measurement, previous studies of oceanic CO emissions utilize empirical gas exchange formulations (e.g., Wanninkhof, 1992; Nightingale et al., 2000). CO solubility in seawater is quite low. Empirical models of air–sea gas exchange typically focus on gases of similarly low solubility (e.g., Rn or He/SF₆ dual tracer methods), so these formulations may also provide a reasonable representation of CO transfer. An eddy correlation flux measurement allows a practical test of this assumption. In a more fundamental sense, direct measurement of the CO flux facilitates development of physical gas transfer algorithms specifying the solubility dependence of the gas exchange coefficient (e.g., Fairall et al., 2011, and references therein).

In this submission we present results from a short field trial of a new method for direct measurement of the oceanic CO flux by eddy correlation. To our knowledge, this is the first reported CO flux measurement from a ship. The data set presented here is brief. Our intent in submitting this article is to (1) present evidence that air–sea flux measurements of CO are feasible with current state-of-the-art instrumentation, and (2) examine flux error related to departure from stationary conditions (see Businger, 1986, for a discussion of stationarity and flux measurement).

2 Experiment

An LGR model 907–0014 N₂O/CO analyzer (Los Gatos Research, Inc.) was used in this trial. This instrument employs a continuous narrow-band infrared laser source for Off-Axis Integrated-Cavity-Output Spectroscopy (OA-ICOS) absorption measurements of N₂O, CO and H₂O (O'Keefe et al., 1999; Baer et al., 2002). In this test, we use a 200-tube Nafion air drier (Perma Pure PD-200T-24-SS) to reduce the dew point to < -10 °C, yielding essentially dry-air concentration values. The analyzer data rate is 10 Hz, but, as we note below, in this configuration at a sample flow of $\sim 10 \, \text{std} \, \text{Lmin}^{-1}$ frequency response is $\sim 1-2$ Hz. Air was subsampled from a 20 m long high-flow Teflon inlet (3/8" ID) drawing air at $\sim 80 \text{ std L min}^{-1}$. The air inlet, sonic anemometer (Gill Model R2) and a six-channel motion sensor (Systron-Donner MotionPak) were mounted at the top of a 10 m meteorological tower on the bow of the University of Hawaii research vessel Kilo Moana. The motion sensor was located 0.6 m below the sonic volume. A short pulse of nitrogen injected at the inlet tip each hour facilitated precise synchronization of wind and CO measurements. Procedures for correcting wind data for ship motion interference have been described previously (Edson et al., 1998; Blomquist et al., 2010).

The mean ten-minute CO variance spectrum (Fig. 1) shows a "pink" background noise ($\sim 1/f^n$) in addition to the -5/3 dependency due to turbulent dissipation. The integrated noise variance over the flux bandpass (0.00167 to 2 Hz) is 0.015 ppb² ($\sigma_{co} = 0.12$ ppb). An instrument artifact signal is evident at 3 Hz, but this is beyond the flux frequency response and has been filtered from the data. A comparison of shipboard spectra with laboratory data (not shown) shows negligible analyzer sensitivity to ship motion.

Fluxes are derived from ten-minute segments of CO and vertical wind velocity data with 50% overlap of successive segments (i.e., 11 ten-minute segments per hour). The linear trend is subtracted from each segment and a Hamming window function applied to limit leakage of low frequency variance unrelated to surface flux. The slope from the linear trend in CO is retained as a measure of $\partial CO/\partial t$ for each segment. Flux is computed as the area of the cospectrum.

This gas inlet has been used extensively for dimethyl sulfide (DMS) flux measurements and the transfer characteristics studied in detail (Blomquist et al., 2010). At flow rates $\geq 80 \text{ Lmin}^{-1}$, frequency attenuation in the main sample line is not significant; the half-power frequency is ~ 10 Hz. The Nafion air dryer produces the greatest signal attenuation, lowering the half-power frequency to ~ 1–2 Hz. The frequency response of the CO analyzer in this configuration is quoted by the manufacturer at 1–2 Hz as well. For DMS, we



Fig. 1. Mean bin-averaged CO variance spectrum for ~ 400 tenminute data segments at sea. Valid data segments were selected using criteria described in Sect. 3. The peak at 3 Hz is an analyzer artifact.

have consistently found a flux attenuation correction of 4-5% at wind speeds comparable to this project (e.g., Yang et al., 2011). We therefore apply the same correction to CO flux. In the future a more thorough examination of flux losses is warranted. However, bias associated with imprecision in this correction is unlikely to alter the conclusions of this report.

Ten-minute flux results are selected to eliminate periods unsuitable for eddy correlation measurements. Data acquisition was continuous, but roughly one-third of the ten-minute flux values over the two-day period were discarded on the basis of selection criteria. Selection limits relating to sampling conditions are: relative wind direction within \pm 60° of the bow, standard deviation in relative wind direction < 10°, and heading change < 25° in ten minutes. In addition, it was necessary to impose stationarity criteria limiting the magnitude of $\partial CO/\partial t$ and horizontal turbulent flux, as described in Sect. 4.

3 Results

The CO flux trial was conducted on a routine cruise to the Hawaii Ocean Time-series (HOT) station ALOHA, located at 22° 45′ N, 158° W (cruise HOT-238, 18–22 December 2011). Over two days of sampling on-station, wind speed was consistently $10-12 \text{ m s}^{-1}$, and relative wind direction remained within $\pm 20^{\circ}$ of the bow. Seawater CO concentration at 5 m depth (Fig. 2) was measured from selected daytime CTD (conductivity, temperature, depth) casts using the method of Xie et al. (2002). An afternoon maximum of ~ 1.5 nM is evident. Nighttime samples were not analyzed but were most likely ≤ 0.5 nM based on data from prior cruises, implying a mean daily concentration of < 1 nM. Seawater CO measurements at station ALOHA on prior cruises since 2008 (also Fig. 2) show a diel pattern typical for blue water regions in the Pacific and Atlantic (e.g., Johnson and Bates,



Fig. 2. Diel cycle in seawater CO at station ALOHA (local time). Crosses: this cruise. Bars: bin-averaged results from previous HOT cruises over all seasons since 2008.

1996; Stubbins et al., 2006; Zafiriou et al., 2008): an early afternoon maximum of 2-3 nM and mean daily concentration of ~ 1 nM. In contrast, peak seawater CO concentrations in Fig. 2 for this trial were about half the typical value, providing a stringent test of the flux measurement method.

Figure 3 is a time series of hourly CO flux for the cruise, computed as the mean of all ten-minute flux measurements each hour meeting selection criteria. Figure 4 shows tenminute results bin-averaged to hour-of-day (local time). The diel cycle in CO flux from Fig. 4 closely mirrors the cycle in seawater concentration in Fig. 2, with a pre-dawn minimum and early afternoon maximum.

For a seawater CO concentration of 1.5 nM at the peak in the flux diel cycle (02:00–03:00 p.m. LT – local time), the CO gas transfer coefficient computed from Eq. (1) at the reference Schmidt number 660 (k_{660}) is 41 cm h⁻¹;

$$k_{660} = \frac{F_{\rm co}}{\alpha_{\rm co} \,\Delta P_{\rm co}} \left(\frac{Sc_{\rm co}}{660}\right)^{1/2},\tag{1}$$

where F_{co} is flux, α_{co} is dimensionless solubility, ΔP_{co} is the interfacial concentration gradient, $(C_{sw}/\alpha - C_{air})$, and Sc_{co} is the Schmidt number in seawater at ambient temperature. For these conditions, at $U_{10} \sim 11 \text{ m s}^{-1}$, the Wanninkhof (1992) gas transfer model gives $k_{660} = 38 \text{ cm h}^{-1}$; Nightingale et al. (2000) gives $k_{660} = 29 \text{ cm h}^{-1}$; McGillis et al. (2001) is $k_{660} = 40 \text{ cm h}^{-1}$; and Woolf (1997) yields $k_{660} = 40 \text{ cm h}^{-1}$ (α , Sc and k_{660} computed using the Rscripts of Johnson, 2010). Clearly, the observed k_{660} is close to the expected value based on several of these models, but with limited data it is difficult to draw too much from this agreement. More extensive sampling of the seawater CO concentration is necessary to critically assess the observed transfer coefficient.



Fig. 3. A time series of hourly mean CO flux over the two-day field test.



Fig. 4. Diel cycle in CO flux over a two-day period at station ALOHA. Error bars are standard error of the mean.

4 Sources of flux uncertainty

Rowe et al. (2011) have analyzed sensor resolution requirements for eddy correlation measurements. For the conditions of this study and the noise level of the CO analyzer, their analysis predicts a 60 % random error for hourly average CO flux measurements at a seawater concentration of 0.5 nM. In this test, however, scatter in hourly CO flux from midnight to 06:00 a.m. LT (when seawater CO is ~ 0.5 nM) suggests a larger error: 0.00063 \pm 0.00118 ppb m s⁻¹ or 187 % as the relative standard deviation.

The expected CO variance from surface flux may be predicted from similarity theory as a function of friction velocity (u_*) and flux magnitude $(|\overline{w'co'}|)$ (Fairall et al., 2000; Blomquist et al., 2010). Assuming neutral stability, the relationship takes the form

$$\sigma_{\rm co,sim} = 3 |w' {\rm co}'| / u_*. \tag{2}$$

As a point of comparison, data for similarity-predicted and observed variance in DMS and CO concentration are shown in Table 1. The observed DMS standard deviation (σ_{obs}) from a cruise in the Sargasso Sea is quite close to the similarity estimate (σ_{sim}). This is reasonable, as the sea surface is the sole

Table 1	 Comparisor 	n of parameters	for DMS and	d CO flux	measure-
ments i	in two field stu	udies.			

Parameter	DMS	СО	Notes
Mean atm. conc. (ppb)	0.100	100	
Atm. lifetime (d)	2-3	50	
Sea-air ΔP (ppb)	6.6	1668	[DMS] = 2.6 nM, [CO] = 1.5 nM
SST (°C)	28	22	
Solubility, α	8.9	0.019	dimensionless liq/gas
$U_{10} ({\rm ms^{-1}})$	6	11	
$k ({\rm cm}{\rm h}^{-1})$	10	45	at ambient SST and Sal
$u_* ({\rm ms^{-1}})$	0.2	0.4	
Flux (ppb m s ^{-1})	0.0016	0.0040	$F = \alpha k \Delta P$
$\sigma_{\rm sim}$ (ppb)	0.021	0.030	from similarity
$\sigma_{\rm obs}$ (ppb)	0.020	0.126	observed minus sensor noise
$\sigma_{\rm sim}/\sigma_{\rm obs}$	1	0.24	



Fig. 5. Trend in $\partial CO/\partial t$ and along-wind (u' co') and cross-wind (v' co') components of horizontal turbulent flux. Data are tenminute values which meet basic sampling criteria. The bounding box shows selection limits, computed here as the 80% confidence limit of the mean in each variable. Results outside the bounding box are excluded on the basis of stationarity criteria, limiting the excessive influence of CO variance from non-surface flux sources.

source of DMS, and its atmospheric lifetime is sufficiently short (2–3 days) to limit the influence of advection from distant sources. However, σ_{obs} for CO is seen to be four times greater than the similarity-predicted value, further suggesting additional CO variance from non-surface-flux sources.

Conditions relating to non-stationarity are an obvious source of additional error. Small gradients in CO concentration can yield variance from horizontal turbulent flux which greatly exceeds variance from surface flux, even for typically clean conditions in the remote marine boundary layer at station ALOHA, where the relative standard deviation in ten-minute mean CO concentration was just 2% over two days on-station. Figure 5 illustrates the relationship between components of the horizontal turbulent flux and $\partial CO/\partial t$. A positive correlation exists between the alongwind component of horizontal flux $(\overline{u'c'})$ and $\partial CO/\partial t$, indicating advection of the CO gradient past the ship. For numerous samples, horizontal turbulent flux is many times larger than the expected magnitude of CO surface flux.



Fig. 6. Mean cospectra illustrating vertical ($\overline{w'co'}$, red) and horizontal ($|\overline{u'co'}|$, blue) CO turbulent flux for ~ 35 selected ten-minute afternoon flux segments (01:00–04:00 p.m. LT). Horizontal flux is computed as the mean of absolute values. After eliminating periods of excessive non-stationarity, the magnitude of horizontal turbulent flux is still several times greater than the vertical flux.

The following additional criteria were therefore applied to eliminate ten-minute segments with excessive gradient influence: $|\partial CO/\partial t| < 2.7 \text{ ppb h}^{-1}$ and $|\overline{u'c'}| < 0.026 \text{ ppb m s}^{-1}$ (shown as a bounding box in Fig. 5).

Even for samples which meet these criteria, the magnitude of $|\overline{u'c'}|$ is large compared to $\overline{w'c'}$. Figure 6 presents cospectra for $\overline{w'c'}$ and $|\overline{u'c'}|$, representing mean fluxes for selected early afternoon ten-minute segments (35 segments, 01:00–04:00 p.m. LT). The $\overline{w'c'}$ cospectrum is positive but noisy due to limited sample size and the effects of residual CO variance from other sources. The integrated area of the $|\overline{u'c'}|$ cospectrum is quite large, with a significant component at low frequencies mirrored in the CO variance spectrum (Fig. 1). The mean absolute horizontal turbulent flux from all ten-minute segments meeting selection criteria ($\langle |\overline{u'c'}| \rangle_{all}$) is 0.008 ppb m s⁻¹ ($\langle \overline{u'c'} \rangle_{all} = -0.0034 \pm 0.0091$ ppb m s⁻¹), or eight times greater than the mean vertical flux ($\langle \overline{w'c'} \rangle_{all}$) of 0.001 ppb m s⁻¹.

The scalar variance budget production term associated with CO turbulent flux in a mean gradient is (Stull, 1988)

$$-2\overline{u_i' \operatorname{co'}} \frac{\partial \overline{\operatorname{CO}}}{\partial x_i},\tag{3}$$

where u_i and x_i specify the full turbulent wind field. From similarity theory, an estimate for the vertical CO gradient is

$$\frac{\partial \overline{\text{CO}}}{\partial z} = -\frac{\overline{w' \text{ co'}}}{\kappa u_* z},\tag{4}$$

which is $\sim 3.5 \times 10^{-4}$ ppb m⁻¹ (0.35 ppb km⁻¹) for mean conditions of this test (i.e., mean flux = 0.001 ppb m s⁻¹; $u_* = 0.4$ m s⁻¹; measurement height, z = 18 m; and the von Karman constant $\kappa = 0.4$). The terms (Eq. 3) for horizontal and vertical flux components are therefore comparable when $\partial \overline{CO} / \partial x \sim 4.3 \times 10^{-5}$ ppb m⁻¹ (4.3 ppb per 100 km). This is a very low threshold gradient for a species with a mean background concentration of 60–150 ppb. Assuming a CO gradient aligned with mean wind at $\overline{u} = 10 \text{ m s}^{-1}$, this corresponds to $|\partial \text{CO}/\partial t| = 1.5 \text{ ppb h}^{-1}$, or approximately half the 2.7 ppb h⁻¹ selection limit. The stationarity criteria therefore limit the variance from horizontal turbulent flux to approximately twice the variance from mean surface flux. In this test, this is sufficient to eliminate the majority of outlier observations.

5 Flux detection limit

To investigate the flux detection limit, we examine theoretical error as a function of air–sea concentration gradient, ΔP_{co} , and wind speed, *u*. Flux error may be specified as a function of variance in both vertical wind (*w*) and scalar (CO) measurements, where CO variance is composed of an atmospheric vertical turbulent flux component ($\sigma_{co_n}^2$) and an "other noise variance" component ($\sigma_{co_n}^2$, from analyzer white noise, etc.), and where *T* is sampling time in seconds (after Fairall et al., 2000).

$$\delta F_{\rm co} = \frac{2\sigma_{\rm w}}{\sqrt{T}} \left[\sigma_{\rm co_a}^2 \, \tau_{\rm w\,co} + \sigma_{\rm co_n}^2 \, \tau_{\rm co_n} \right]^{1/2} \tag{5}$$

The two terms in Eq. (5) are assumed to be independent, with characteristic integral time scales (τ). From nighttime flux measurements under conditions where ΔP_{co} is very low (and therefore $\sigma_{co_a}^2 \sim 0$), we can solve Eq. (5) for the "other noise" term, yielding $\sigma_{co_n}^2 \tau_{co_n} = 0.00041$. Using similarity relationships to represent $\sigma_{co_a}^2$, σ_w and τ_{wco} , and employing empirical functions for the stability dependence of these parameters (see Blomquist et al., 2010) yields an expression for error as a function of u and u_* , which can be further extended to the following relationship for $\Delta P_{co}(u)$ (Eq. 6) by assuming an arbitrary error condition (e.g., $\delta F/F = 1$, or 100% error) and substitution of the standard flux formulation: $F_{co} = \alpha k(u) \Delta P_{co}$.

$$\Delta P_{\rm co}(u) = \frac{2 \times 1.25 \, u_* \, f_{\rm w}(z/L)}{\alpha k(u) \sqrt{3600}} \left[\left(\frac{3 \, F_{\rm co} \, f_{\rm c}(z/L)}{u_*(u)} \right)^2 \\ \frac{2.8 \, z \, f_{\tau}(z/L)}{\overline{u_{\rm r}}} + 0.00041 \right]^{1/2} \tag{6}$$

Here, $f_i(z/L)$ are functions defining stability dependence (unity for neutral conditions assumed here), $\overline{u_r}$ is mean relative wind speed (equivalent to \overline{u} if the ship is not moving), and k(u) is the gas transfer coefficient function. For CO, k(u) may be estimated from a cubic wind speed dependence (e.g., Edson et al., 2011). An estimate for $u_*(u)$ may be obtained by assuming a roughness length typical of the open ocean (~ 0.0003 m), or by a fit to observed u_* , or from a fit to bulk flux model derived u_* (e.g., COARE 3.0). Note that in Eq. (6), F_{co} is dependent on ΔP_{co} and u, so an iterative



Fig. 7. The flux detection limit criterion expressed as ΔP_{co} ppb for $\delta F/F = 1$ (100 % error in observed CO flux) versus wind speed for 1 h sampling time under neutral stationary conditions.

solution is necessary. Alternately, Eq. (6) may be further rearranged and solved for ΔP_{co} following substitution for F_{co} .

The detection limit criterion $\Delta P_{co}(u)$ computed from Eq. (6) is shown in Fig. 7. This curve should be a theoretical limit under neutral stationary conditions (the similarity functions assume stationarity), but in fact it may be an upper limit, as $\sigma_{co_a}^2$ is not exactly zero in the empirical determination of the "other error" term above. We also note that, other things being equal, as SST (sea surface temperature) decreases so does ΔP_{co} , and therefore flux error increases.

Early afternoon conditions for this field trial $(\Delta P_{co} = 1700 \text{ ppb}, u = 11 \text{ m s}^{-1})$ lie a factor of three above the curve in Fig. 7, implying an expected error of 33% for hourly mean flux at the peak in the diel cycle. This is approximately the observed error from Fig. 4 (22–37% relative error at 01:00–03:00 p.m.LT). Results in Fig. 4 represent the average of all 10-min flux measurements for each hour which meet selection criteria, and in this case the afternoon values include only a little more than one hour of total sampling time, which is approximately the sampling time assumed in Fig. 7. The detection limit presented in Fig. 7 supports the conclusion that oceanic CO flux measurements are feasible under favorable conditions with appropriate selection criteria.

6 Conclusions

The analytical performance of a commercially available infrared OA-ICOS trace gas analyzer is sufficient for shipbased flux measurements of CO at moderate-to-high wind speeds when seawater concentration is > 1 nM. A clear diel cycle in CO flux, mirroring the cycle in seawater concentration, was observed over two days at a research site near Oahu in the oligotrophic North Pacific subtropical gyre. CO flux measurements by eddy correlation demonstrated here are a potentially important development for studies of biogeochemical and physical dynamics in the ocean's surface mixed layer. Additionally, CO is an important low solubility end-member in the spectrum of gases involved in air– sea exchange. As such, it should exhibit significant bubblemediated gas exchange enhancement at moderate-to-high wind speeds, providing an interesting and important test of physical gas transfer theory.

The effects of non-stationarity are clearly significant for CO. The moderately long atmospheric lifetime of CO (~50 days), combined with vigorous natural and anthropogenic sources, yields a high, variable background atmospheric concentration of ~100 ppb in the Northern Hemisphere and half that value in the Southern Hemisphere. CO variance from horizontal turbulent diffusion of atmospheric gradients as small as 1-2% of the mean concentration per 100 km reduces precision of the eddy correlation flux measurement. Removing 10-min flux values which exhibit excessive horizontal flux or $\partial CO/\partial t$ (Fig. 5) is critical to reducing error to near the theoretical limit and resolving the diel cycle in CO flux. These conclusions may also apply to flux measurements of other long-lived gases with high mean background concentrations.

In practice, ideal stationarity is never realized in the field and the question "How much non-stationarity is too much?" is an interesting one. The answer probably depends on the nature of the scalar and the scientific question to be addressed. Criteria are often somewhat subjective. In this case, flux data in Fig. 5 show a clear central cluster surrounded by a widely scattered cloud of outliers. Limits were chosen to include the densest portion of the central cluster. Furthermore, it is apparent from Fig. 5 that $\partial CO/\partial t$ shows the greatest range as an indicator of non-stationary conditions, but it is not always sufficient. Some samples exhibit significant horizontal turbulent flux and low $\partial CO/\partial t$. It therefore seems wise to examine stationarity from a variety of perspectives. These considerations may impose stringent location selection criteria for future CO air-sea flux studies. On the basis of this test, conditions at station ALOHA appear suitable and many locations in the Southern Hemisphere should be equally acceptable.

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